

HIGH ALTITUDE HVAC DESIGN CONSIDERATIONS Goals NOT Overview Cookbook ❖ Substitute for ❖ A Few Examples engineering ❖ Thought Process **❖**Why ❖(In the words of...) Understand, rather than..... May 10, 2019 [©] Michael D. Haughey, P.E., CEM, HBDP, LEED AP High Altitude HVAC Design 2 RM ASHRAE - 2019 Tech Conf

Altitude Effects Understanding Why

- Baseball
 - ❖ Home run distance
 - ❖ Curve ball
- Basketball
 - ❖ Doug Moe Era
- Football
 - ❖ Field goal distance

- · Similarities???
 - Relation to air density
 - ❖ Gravity???
 - Function of oxygen content
 - ❖ Heat Rejection
 - ➤ Sensible?
 - ➤ Latent?

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Mitigating Factors

- Equipment counteracts using:
- ❖ Humidity
- ❖ Temperature
- Heat transfer

❖ Pressure

Equipment design basis

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Altitude Dependent System/ Equipment Examples

- Airflow calculations
- Fans, ductwork (sizing, pressure)
- Air-cooled equipment
 - > Condensers, chillers
 - Motors, electrical and electronic equipment

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- Combustion equipment
 - ➤ Boilers, furnaces, generators, engines, gas absorption
- Pumps
- Evaporative coolers, Cooling towers
- Balancing, VAV box

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Altitude Dependent System/ Equipment Examples

- New 2017
 - ❖ Desiccant Dehumidification
- New 2019
 - **❖** Boilers

- New 2018
 - ❖Snow Entrainment
 - Load calculations

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Airflow Calculations - (Sensible Only)

- cfm = (Btu / hr) / $(C_P * p * 60 * DT)$
- Let C_P * p * 60 = F_{CFM}

F_{CFM} = "CFM transfer factor"

cfm = (Btu / hr) / (F_{CFM} * DT)

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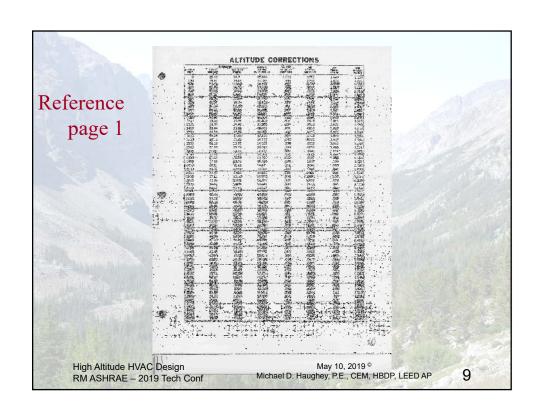
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Airflow Calculations - (Sensible Only)

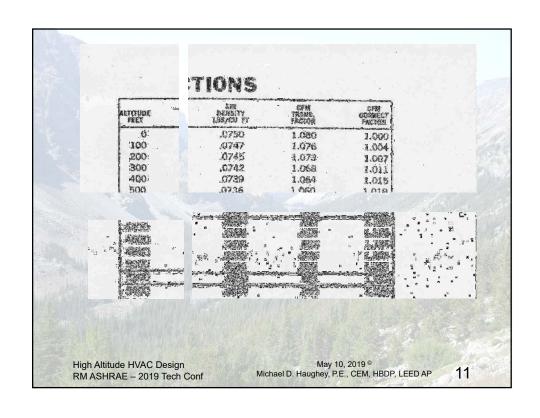
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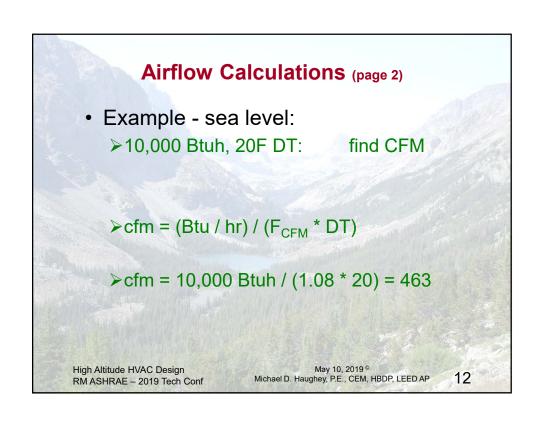
- cfm * F_{CFM} * DT = Btu / hr
- Look up F_{CFM} in tables (handout, 1st page). THEN
- Check on Psych Chart

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		METER	SPECIFIC	REL DEN	AIR DENSITY	CFM	CFM
FEET	INCHES MERCURY	LBS/SQ IN ATMOS.	CU FT PER LB	SP OR HP CORR FACT	LBS/CU FT	CFM TRANS. FACTOR	CORRECT
0	29.92	14.7	13.340	1.000	.0750	1.080	1.000
100	29.81	14.64	13.389	.996	.0747	1.076	1.004
200	29.70	14.58	13.439	.993	.0745	1.073	1.007
300	29.60	14.52	13.488	.989	.0742	1.068	1.011
400	29.49	14.46	13.538	.985	.0739	1.064	1.015
500	29.38	14.40	13.587	.981	.0736	1.060	1.019
600	29.28	14.36	13.636	.978	.0734	1.057	1.022
700	29.17	14.32	13.686	.975	.0731	1.053	1.026
800	29.06	14.28	13.735	.971	.0728	1.048	1.030
900	28.96	14.24	13.785	.967	.0725	1.044	1.034
1000	28.85	14.20	13.834	.964	.0723	1.041	1.037
1100	28.75	14.14	13.883	.960	.0720	1.037	1.041
1200	28.65	14.08	13.933	.957	.0818	1.034	1.045
1300	28.54	14.02	13.982	.954	.0716	1.031	1.049
1400	28.44	13.96	14.031	.951	.0713	1.027	1.052
1500	28.33	13.90	14.081	.947	.0710	1.022	1.05€
1600	28.23	13.86	14.130	.944	.0708	1.020	1.060
1700	28.13	13.82	14.179	.940	.0705	1.015	1.064
1800	28.02	13.78	14.228	.936	.0702	1.011	1.068
1900	27.92	13.74	14.278	.933	.0700	1.008	1.071
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Airflow Calculations (page 3)

- Example 5,200 ft. elevation >10,000 Btuh, 20F DT
 - \gt cfm = (Btu / hr) / ($F_{CFM} * DT$)
 - >cfm = 10,000 Btuh / (0.891 * 20) = 561
 - Note, for simplicity, many applications are close enough using 0.9 in lieu of 0.891

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Standard and Actual Air

- Standard air, SCFM, is at sea level and 70°F
- Actual air, ACFM, is at actual conditions
- To convert, correct for density change due to both altitude and temperature
- For altitude: SCFM
 = ACFM * (density ratio)
- Example, 1000 CFM at 5,200 ft. elevation (equiv. mass):
 - > 825 SCFM = 1,000 ACFM * 0.825

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Fan and Duct System Pressure Drop Calculations (Example)

- Separate items using sea level data from items using altitude data (e.g. duct friction)
- Example (5,200 ft. elevation, 10,000 CFM)

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Example (5,200 ft. elevation, 10,000 CFM)

	Sea level DP " w.c.	Alt. DP
Cooling coil (computer sel.)		0.6
Heating coil (computer sel.)		0.2
Ductwork (ductilator)	1.5	
Fittings (ASHRAE tables)	2.0	
Other (diffuser, louvers, dampe	ers) 1.5	
<u>-</u> Total	5.0	0.8
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Example (5,200 ft. elevation, 10,000 CFM) (page 2)

- (example continued)
 - ➤ Correct sea level items:
 - ➤ Density ratio = 0.825 at 5200 ft
 - >5.0 * 0.825 = 4.125
 - ightharpoonupTotal = 4.125 + 0.8 = 4.925 at alt.
 - >At sea level = 4.925/.825 = 6"
- Fan selection chart SL or Alt?
- Use computer selection at altitude, OR

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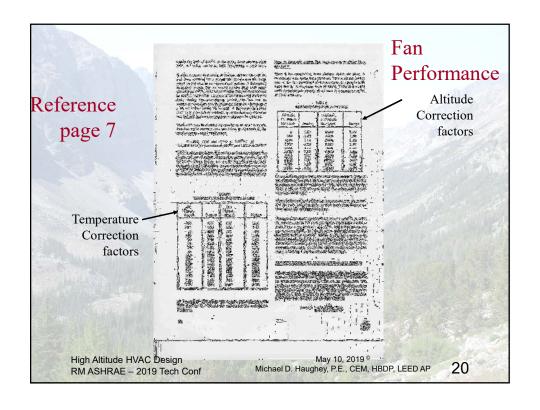
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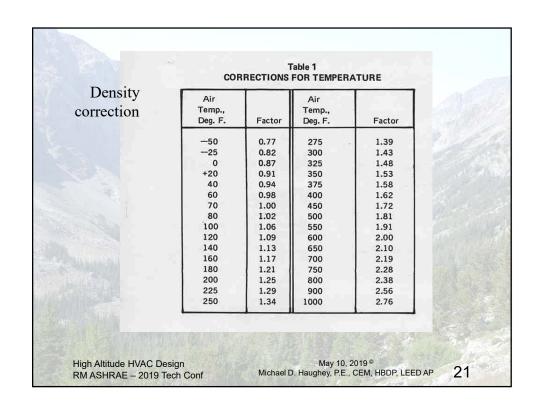
Example (5,200 ft. elevation, 10,000 CFM) (page 3)

- Select from sea level tables or graphs:
 - ➤ RPM is the same at higher altitude (e.g. 1200 RPM)
 - ➤ CFM is the same at higher altitude (e.g. 10,000 CFM)
 - Correct brake horsepower by density ratio, for example 10 HP from sea level chart becomes 10 * 0.825 = 8.25 at 5,200 ft. altitude
- (More on pg. 7 of handout)

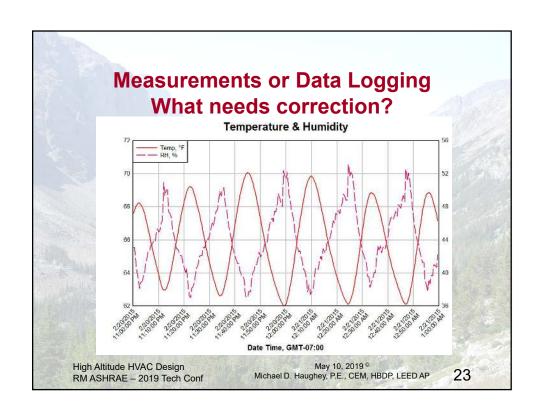
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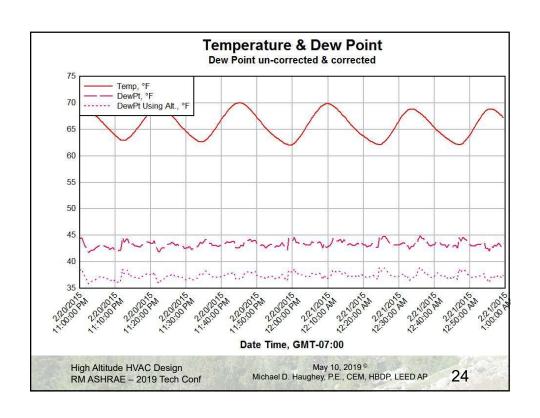
Fan and Duct System Calculations (page 4) • The selection is thus 10,000 CFM, 1200 RPM, 4.9" s.p., AT 5200 FT. ALTITUDE – or • 10,000 CFM, 1200 RPM, 6.0" s.p., AT SEA LEVEL • Remember, derate the motor due to less motor cooling at higher altitude and add appropriate safety factors High Altitude HVAC Design May 10, 2019 and 2019 Tech Conf Michael D. Haughey, P.E., CEM, HBDP, LEED AP 19

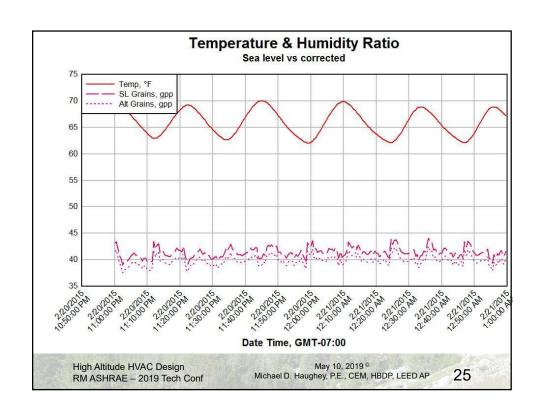




C		Table 2 NS FOR ALTITU	JDE	Densi
Altitude, Ft. Above Sea Level	Factor	Altitude, Ft. Above Sea Level	Factor	correction
0	1.00	5000	1.20	
500	1.02	5500	1.22	
1000	1.04	6000	1.25	
1500	1.06	6500	1.27	
2000	1.08	7000	1.30	
2500	1.10	7500	1.32	
3000	1.12	8000	1.35	
3500	1.14	8500	1.37	
4000	1.16	9000	1.40	
4500	1.18	10000	1.45	







Desiccant Dehumidification

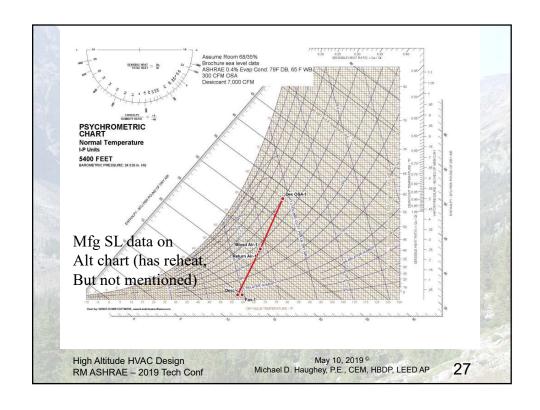
- Function of mass transfer & heat transfer, plus ...
- · Air is less dense at altitude
 - **.**Less dehumidification capacity

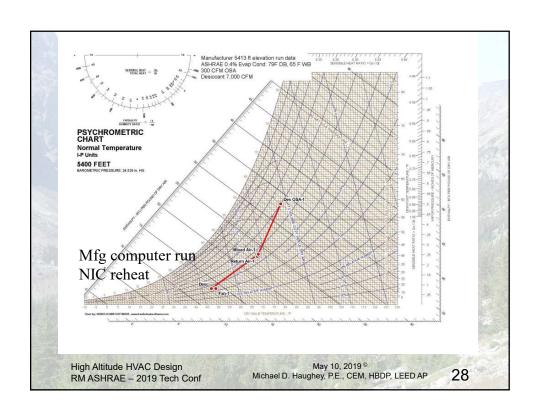
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- Use manufacturer's data if avail & if trust
- Otherwise, approx.: try derate of latent capacity by density ratio
 - ❖ Plot on psych chart using same CFM to determine dew point, etc.

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Desiccant Dehumidification

- Verify if data includes reheat
- Example
- Sea Level data plotted on Alt chart
 - ❖ 164 MBH latent
 - ❖231 MBH total
- 5400 ft Air density ratio: 0.819

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- Mfg run at alt plotted on psych chart
 - ❖ 124 MBH latent
 - ❖256 MBH total
- Note: SL data from Lit includes internal reheat. Mfg run above does not.
- Ratio, Latent: 0.756

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Snow Entrainment; Louvers

- High Altitude Consideration
 - Density, moisture content
 - Hard to capture & melt especially higher and colder environment
 - ❖ Ice crystals

- No hard rules, except one:
 - The space the architect allocated for louvers isn't enough

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Snow Entrainment Louvers Guidelines

- Space to let snow drop out
- · Space to melt
- Something to stop snow – not paper filters
- Easy access for frequent unplugging

- Location, location, location
- Typ 400 to 700 fpm Free area velocity, but won't stop light or wind-driven snow

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Load Calculations: solar load Older data

- Due to altitude and location, a clearness factor of at least 1.15 is recommended (ASHRAE Applications, Chapter 33, Figure 5).
- https://en.wikipedia. org/wiki/Air mass %28solar energy% 29

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Load Calculations: solar load Newer Data

- ASHRAE location data
- · Monthly noon:
 - clear sky beam & diffuse optical depth
 - clear sky normal & diffuse horizontal irradiation (radiative energy flux)

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Load Calculations (solar load):

- Using interpolation between stations
- Adjust for altitude
 - Call load program author
 - ❖ Guess at 2% to 3% per 1000 ft
- Adjust for cloudiness, pollution, local shading, humidity, ...

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Condensers, Air-cooled Chillers

- Packaged equipment:
 - Lower air density = less heat rejection = higher temperatures = more heat rejection
 - ➤ Therefore, counteracting forces. Net capacity reduction is typically less than air density ratio

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Packaged equipment (page 2)

- Function of specific equipment design, refrigerant pressures, operating conditions, etc. Use manufacturer published corrections for altitude or call the manufacturer.
- Note in one Mfg's literature that correction factors for 5000 ft. elevation for air cooled condensers is 0.90 and for air cooled chillers is 0.97 for SPECIFIC series of equipment.

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Air-cooled Chillers (page 1)

- Note Mfg A, Model B chiller data lists an 0.97 capacity correction factor for 6000 ft. altitude.
- Get the data for your specific application and selection if you need the accuracy.

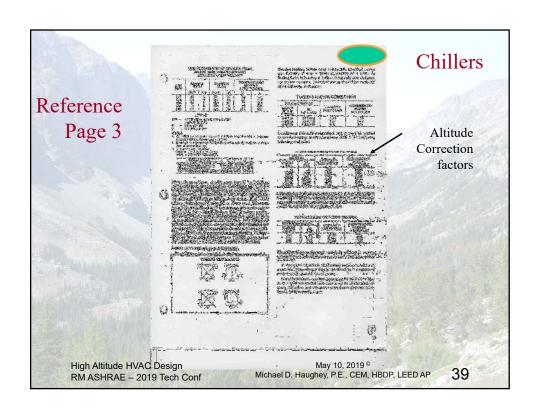
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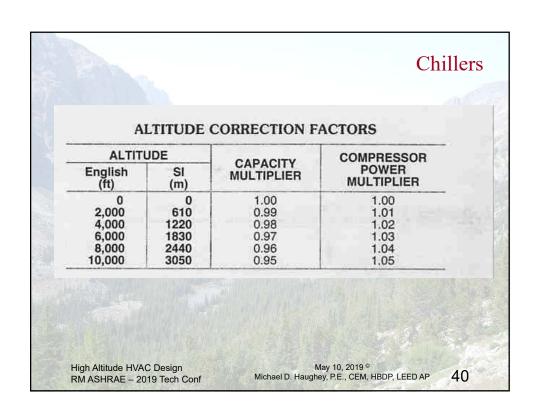
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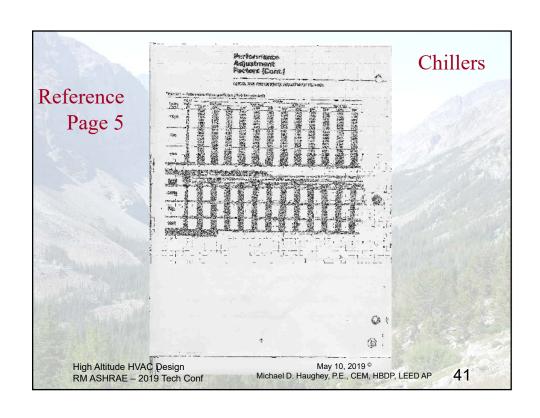
Air-cooled Chillers (page 2)

- Mfg C, Model D
 literature lists
 capacity correction
 factors which
 combine fouling
 factor, chilled water
 DT, and altitude,
- and varies from 0.871 to 0.96 for 6000 ft. altitude. The correction from the standard condition (sea level, 10F DT, 0.00025 fouling factor, is 0.94.

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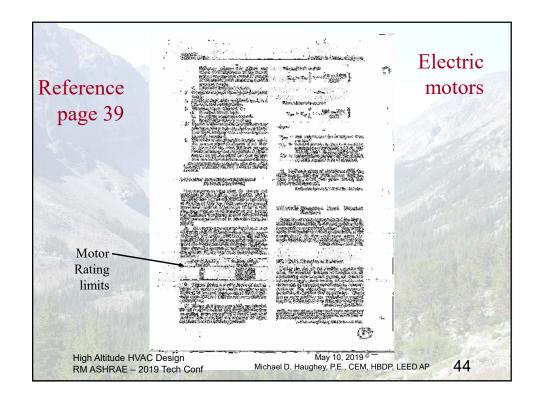


	Chilled						Alt	itude		
Fouling	Water		Sea Level			2,000 Feet			4,000 Feet	
Factor	ΔΤ	CAP	GPM	KW	CAP	GPM	KW	CAP	GPM	KV
	6	0.987	1.650	0.993	0.967	1.640	1.003	0.952	1.620	1.0
0.00025	8	0.993	1.250	0.997	0.973	1.240	1.007	0.956	1.220	1.02
0.00025	10	1.000	1.000	1.000	0.980	0.990	1.010	0.960	0.970	1.03
	12	1.007	0.820	1.003	0.987	0.810	1.013	0.966	0.800	1.03
	14 16	1.013	0.710	1.007	0.993	0.700	1.017	0.972	0.680	1.03
		1.020	0.640	1.010	1.000	0.630	1.020	0.980	0.620	1.04
	6	0.957	1.615	0.979	0.953	1.600	0.989	0.931	1.570	0.99
0.001	8	0.964	1.215	0.982	0.959	1.210	0.992	0.937	1.180	0.99
0.001	10	0.970	0.965	0.985	0.964	0.960	0.995	0.943	0.940	0.99
	12	0.976	0.785	0.989	0.966	0.790	0.998	0.945	0.770	1.00
	14	0.982	0.675	0.993	0.968	0.670	1.001	0.947	0.650	1.01
	16	0.989	0.620	0.996	0.970	0.600	1.004	0.949	0.590	1.02
	6	0.916	1.565	0.951	0.913	1.550	-			
(action of the			1.245	0.958						0.97
0.002			0.925	0.965						0.97
			0.810	0.969						0.98
			0.695	0.973						0.98
	16	0.948	0.580	0.976	0.931	0.580				0.98
0.002	8 10 12 14 16	0.923 0.930 0.934 0.938 0.948	1.245 0.925 0.810	0.958 0.965 0.969 0.973	0.919 0.925 0.927 0.929	1.170 0.920 0.750 0.640	0.969 0.972 0.975 0.978 0.981 0.983	0.896 0.898 0.900 0.908 0.916 0.924	1.490 1.110 0.890 0.730 0.620 0.580	0

Air-cooled Electric Motors

- Limited by allowable temperature
- Higher altitude = less air = less cooling = lower rated capacity
- Standard motors rated at 1,000 meters (3,300 ft.) altitude
- Again, manufacturer's design details are a factor. When critical, get data from the selected manufacturer.

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Electric motors

Motors with Class A or B insulation altitude rating increases as ambient temperature is lowered

Ambient Temperature, Degrees C	Maximum Altitude, Feet (Meters)
40	3300 (1000)
30	6600 (2000)
20	9900 (3000)

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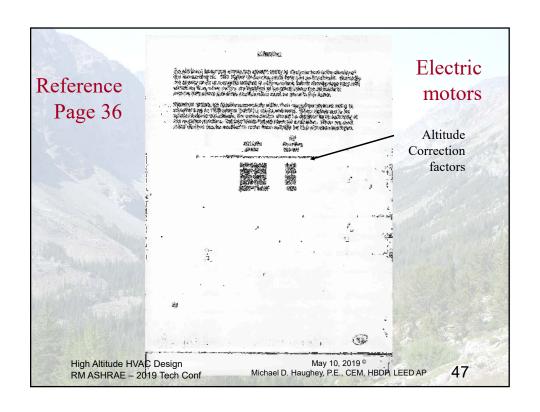
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Air-cooled Electric Motors (page 2)

- ANSI / NEMA Standard MG-1
 - Motors rated at 40C which are intended for use above 1000 meters should have the allowable temperature rise reduced in accordance with mfg's formula

Mfg E listed a correction factor for their Model F induction motor of 0.94 at altitudes from 5,001 ft. to 6,600 ft.

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	Altitude (feet)	HP Derating Factor	Electric
	3,300-5,000	0.97	
	5,001-6,600	0.94	
	6,601-8,300	0.90	
	8,301-9,900	0.86	
	9,901-11,500	0.82	
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Combustion Equipment

- Gravity, packaged equipment, AGA: de-rate by 4% / 1,000 ft. (volume of combustion air & flue gas increases about 4%/1,000 ft.)
 - ➤ Typically de-rate when above 2,000 ft. elevation

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- Often reduce gas orifice size to match gas input to altitude air
- Some boiler manufacturers have condensing boilers with "lower altitude derates".

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Combustion Equipment (page 2)

- Design Options
 - Decrease gas manifold pressure
 - Increase gas orifice pressure loss (smaller orifices)
 - Increase airflow (mass flow) with power burner fan, forced draft fan, or induced draft fan

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Combustion Equipment (page 3)

- **Gas Heat Content**
 - > Reduces according to the air density
 - ➤ Typically 1,000 BTU per Cu. Ft. at sea level, 830 BTU per Cu. Ft. at 5,000 ft. altitude, etc.
- Some utilities vary the heat content, therefore call the utility for the specific location. Some increase the heat content to achieve 1,000 BTU per Cu. Ft. at 5,000 ft. altitude.

(see "Boiler House Journal", near end of handout)

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Hugo, CO vs. Denver

Altitude 5046

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- 5200
- Rel density: 0.830
- 0.825
- Btu content: 780
- 831

SG: 0.65

- 0.67
- · Peoples Gas
- Company
- Excel Energy

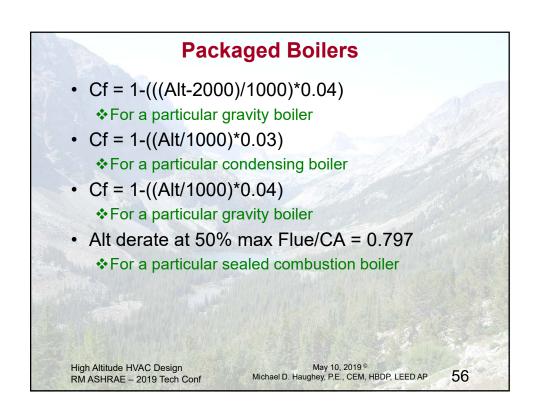
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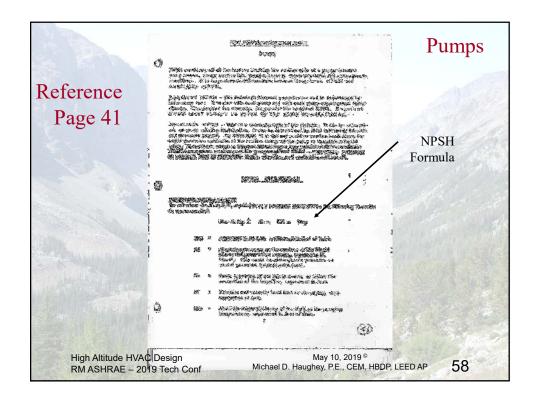
Las Animas, CO vs. Denver Altitude: 3901 • 5200 • Rel density: 0.867 • 0.825 Btu content: 735 • 831 • SG: 0.62 • 0.67 Citizen's Utility Excel Energy Company ❖ Internet search – not found ❖Black Hills Energy? High Altitude HVAC Design May 10, 2019 © 53 RM ASHRAE - 2019 Tech Conf Michael D. Haughey, P.E., CEM, HBDP, LEED AP

Combustion Equipment (page 4) · Flue Design > Available draft decreases substantially at higher altitudes > Follow the manufacturer's procedures or ASHRAE procedures, which account for altitude barometric pressure May 10, 2019 [©] Michael D. Haughey, P.E., CEM, HBDP, LEED AP High Altitude HVAC Design 54 RM ASHRAE - 2019 Tech Conf

Boiler Options				
Altitude	e: 7800			
Load without mo	rning			
warmup		Boiler R	Boiler Rating	
		Alt	Eff	
Existing Boiler:	Mfg A Model A Gravity	0.768	0.82	
Mfg A Model A		0.768	0.82	
Mfg B Model A	-	0.766	0.95	
	High Altitude Condensing	1	0.95	
Mfg C Model A		0.766	0.95	
	cast iron - copper fin tube	0.688	0.85	
Mfg D Model A		0.768	0.82	
Mfg E Model A		0.768	0.833	
Cast Iron mode	els, high eff:			
Not available				
Sealed Combu	stion, modulating:			
Mfg B Model C	No longer made?	0.688	0.85	
Mfg F Model A	A little too small with alt derate	0.768	0.88	
	Alt derate at 50% max Flue/CA	0.797	0.88	



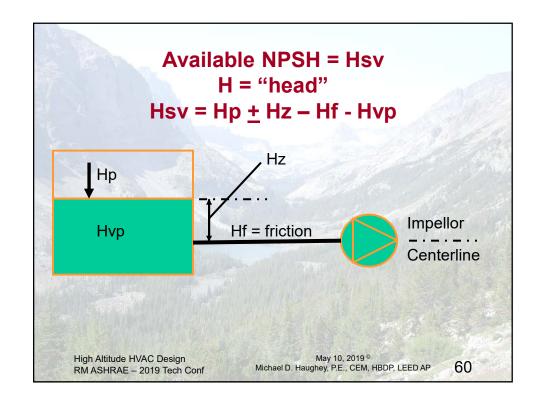
Pumps NPSH: less Three concerns: barometric pressure > NPSH on open systems, 6 ➤ Cavitation ft. less at 5000 ft. ➤ Motor cooling / rating altitude All are air density · Cavitation: less related barometric pressure ❖ Use the standard on open systems formulas with actual barometric pressure data May 10, 2019 [©] Michael D. Haughey, P.E., CEM, HBDP, LEED AP High Altitude HVAC Design 57 RM ASHRAE - 2019 Tech Conf



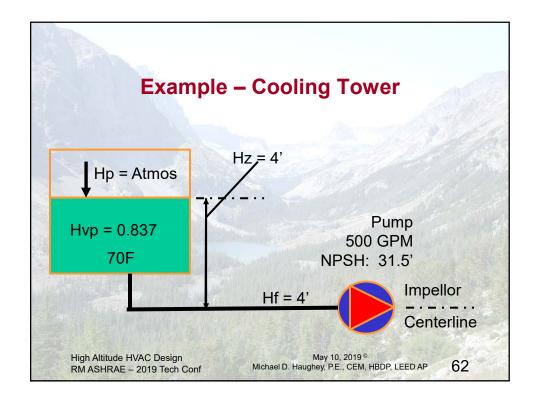
NPSH

- Hsv = available NPSH in ft of fluid
- Hp = absolute pressure on liquid surface, ft
- Hz = height of liquid surface above impellor centerline, ft
- Hf = friction and velocity head loss, ft
- Hvp = absolute vapor pressure at pumping temperature, ft

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 $Hsv = Hp \pm Hz - Hf -$ Available N. P. S. H. expressed in feet of fluid. Hsv = Hp Absolute pressure on the surface of the liquid where the pump takes suction, expressed in "feet". This could be atmospheric pressure or vessel pressure (pressurized tank). Static elevation of the liquid above, or below the Hzcenterline of the impeller, expressed in feet. Hf Friction and velocity head loss in the piping, also expressed in feet. Hvp Absolute vapor pressure of the fluid at the pumping temperature, expressed in feet of fluid. High Altitude HVAC Design May 10, 2019 © 61 Michael D. Haughey, P.E., CEM, HBDP, LEED AP RM ASHRAE - 2019 Tech Conf



Hsv = Hp + Hz - Hf - Hvp

Sea Level

$$4 \text{Hsv} = 34' + 4' - 4' - 1' = 33'$$

- *OK
- 5000 ft

$$+$$
 Hsv = 28' + 4' - 4' - 1' = 27'

❖ Will cavitate

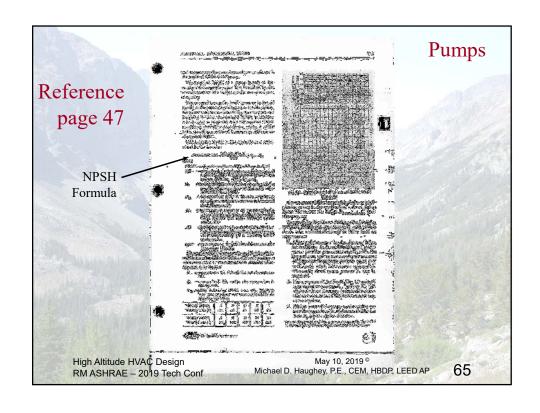
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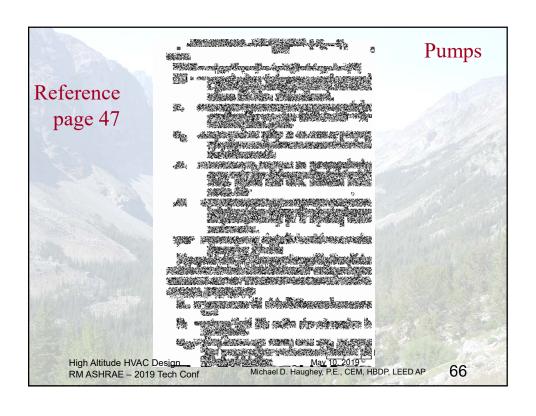
63

Another NPSH Formula

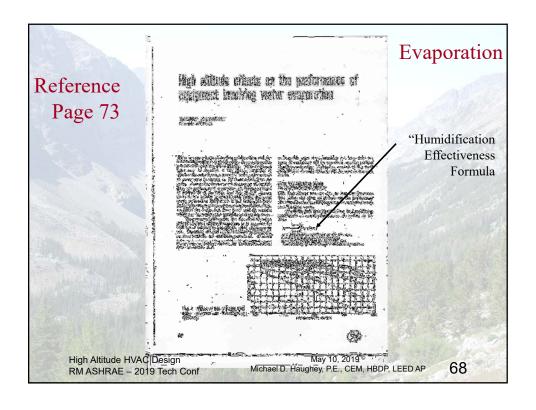
- For your homework
- Use the formula on Reference page 47

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Evaporative Coolers Significant Density and heat **Parameters** transfer coefficient and vapor pressure ➤ Mass Velocity effects are ➤ Air Density compensating > Heat Transfer Coefficient, ❖ Data hard to find, turbulence at typically not derated boundary layer for altitude > Water Vapor Accurate selections Pressure typically not needed May 10, 2019 © High Altitude HVAC Design 67 Michael D. Haughey, P.E., CEM, HBDP, LEED AP RM ASHRAE - 2019 Tech Conf



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Effectiveness Evaporation

\eta = \frac{t_B - t_L}{t_E - t'}, \text{ where} \\
\eta = \text{humidifying efficiency or effectiveness,} \\
t_B = \text{entering dry-bulb temperature,} \\
t_L = \text{leaving dry-bulb temperature,} \text{ and} \\
t' = \text{entering (and leaving) wet-bulb temperature.}

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Cooling Towers • Some controversy before computer selections • Don't derate but increase fan motor HP • Don't derate • Don't derate and reduce fan motor HP • Add capacity at higher altitude High Altitude HVAC Design May 10, 2019 Michael D. Haughey, P.E., CEM, HBDP, LEED AP 70

Cooling Towers

- For some (or most typical, higher WB)
 operating conditions, increased water
 partial pressure at higher altitudes may
 have a greater effect in increasing
 capacity than reduced density does in
 reducing capacity
- Cold air operation economizers: less capacity.

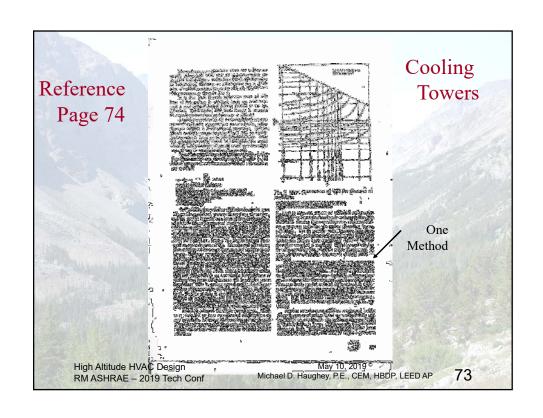
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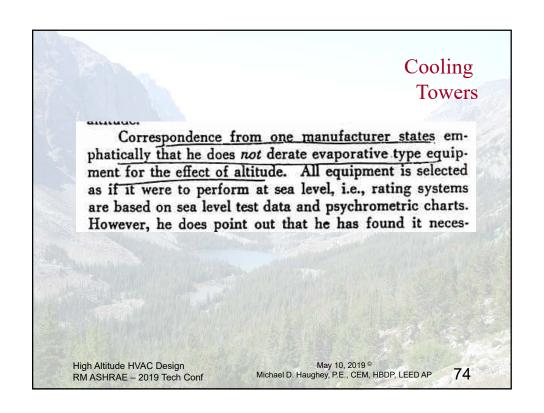
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Cooling Towers

- Data hard to find, normally included in selection software
- Some info at CTI.org/tech_papers

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Cooling Towers (page 2)

- Increased capacity factor due to increased enthalpy at higher altitudes is more pronounced at higher entering wetbulb temperature.
- Per one manufacturer's representative, 1/2% per 1000 ft. for 65F EWB and 1.25% per 1000 ft. for 78°F EWB.

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Cooling Towers (page 3)

- What about much lower EWB, such as hydronic economizer applications???
- Lower density overpowers the added capacity from increased vapor pressure at higher altitude
- Therefore at lower temperatures there is a net reduction in capacity

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Summary

- Use Mfg data where available, BUT check it to be sure reasonable
- Consider
 - ❖ density
 - ❖ Heat transfer
 - ❖ Motor cooling
 - ❖ Vapor pressure
 - ❖ Mass flow

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- Be aware of counteracting factors
- Use altitude psych charts
- Be sure of the altitude for data
- Use absolute barometric pres.

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